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SOLAR/2017-79/05

### Monthly Performance Report

ALABAMA POWER COMPANY

MAY 1979



U.S. Department of Energy

National Solar Heating and Cooling Demonstration Program

National Solar Data Program

### NOTICE \_\_

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### MONTHLY PERFORMANCE REPORT ALABAMA POWER COMPANY MAY 1979

### I. SYSTEM DESCRIPTION

The Alabama Power Company solar energy site is a two and one-half story commercial office building located in Montevallo, Alabama. The building has a floor area of approximately 17,000 square feet. The solar energy system is designed to provide 57 percent of the annual domestic hot water and space heating demands and up to 18 percent of the annual space cooling demand.

The collector subsystem includes four rows of flat plate double glazed collectors. The gross area of the collectors is 2,340 square feet. The collectors are supplemented by two types of reflectors. The rear three rows of the collectors have facing mirrors sloped at 45 degrees from the horizontal while the collectors are sloped at 30 degrees from the horizontal, facing south. All four rows of collectors have vertical mirrors mounted at the tops of the collector frames. The total area of the sloped reflectors is 2,250 square feet and the total area of the vertical reflectors is 740 square feet. The collection transport fluid is water and a drain down method of freeze protection is used. An 8,000 gallon tank is used to store solar energy.

Domestic hot water (DHW) preheating is accomplished by means of a heat exchanger tube passing through the solar storage tank. Solar preheating is supplemented, as required, by a 120-gallon electric water heater.

There are seven independently controlled heating/cooling zones. Each zone is supplied by its own air-handling unit. The air handling units have both hot and cold water lines to allow each unit to be used and controlled independently of the other six parallel units.

Space heating is provided by pumping water from the solar storage tank through heating coils in the air-handling units. The water from solar storage is passed through an electric auxiliary boiler prior to entering the coils of the air-handling units. If the water temperature in the

solar storage tank is too low to meet the heating demand, the electric boiler is used to provide additional heating to the water, as required.

Solar energy used in cooling is provided by passing water directly from the collectors to the generator section of a 25-ton absorption chiller. Auxiliary cooling is provided by a 30-ton electric reciprocating chiller which is used in parallel with the absorption machine. An 8,000-gallon chilled water storage tank is also included in the system. This chilled water storage tank can be supplied by the absorption machine or by the reciprocating chiller during off-peak hours.

The system, shown schematically in Figure 1, has four modes of solar operation.

Mode 1 - Collector to Storage: This mode is enabled by a time clock during daylight hours and it is entered when the temperature of the water at the collector outlet exceeds the temperature of the water in the solar storage tank by approximately 10°F. This temperature differential is adjustable and is to be adjusted for optimum performance based on operational experience. The mode is terminated when the collector outlet temperature no longer exceeds the storage tank temperature by the adjusted value or when the time clock disables the mode logic.

Mode 2 - Collector to Cooling: This mode is entered out of Mode 1 when the collector outlet water temperature reaches or exceeds 165°F. Water from the collectors is diverted directly to the generator section of the absorption chiller before returning to solar storage. Evaporator outlet water is passed to the cooling coils in the air handlers whenever a cooling demand exists. If no cooling demand exists during this mode, the chilled water from the absorption machine passes into the chilled water storage tank. In this mode, the absorption machine functions in parallel with the electric chiller to supply the building cooling load. Since heating and cooling are independently controlled by each zone, it is possible to have this mode and Mode 3 active simultaneously. The mode is terminated when the absorption machine generator inlet water temperature drops to 157°F.

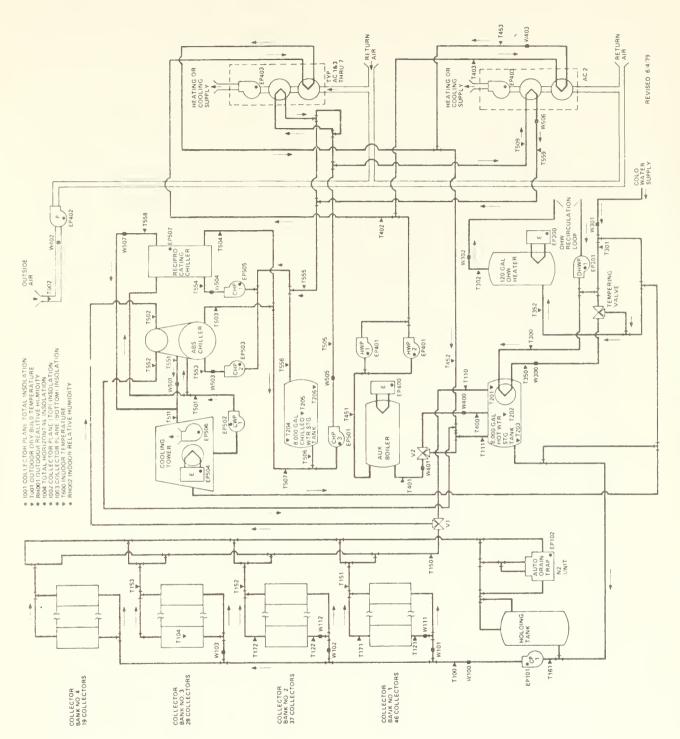


Figure 1. ALABAMA POWER SOLAR ENERGY SYSTEM SCHEMATIC

Mode 3 - Storage to Space Heating: This mode is initiated when a demand for space heating occurs at any of the independently controlled heating/cooling zones or when the outdoor air temperature drops below 65°F. Water from the solar storage tank is pumped through the auxiliary boiler, out to the air handling units and returned to storage. If the temperature of the water in the solar storage tank is above the limit value of 140°F, blending of solar storage water and space heating return water occurs to maintain a boiler inlet water temperature below 140°F. The minimum control temperature for space heating supply is varied with outside air temperature. When the outside air temperature is 65°F, the minimum space heating water temperature is 80°F. When the outside air temperature is 25°F, the minimum space heating water temperature is 120°F. The boiler is activated, as required, to maintain the minimum space heating temperature according to the control temperature just described. If the solar storage tank temperature is below the temperature of the space heating return water, the solar storage tank is bypassed by the return water. This mode can be active simultaneously with Mode 2 since heating and cooling demands are independently determined by each of the heating/cooling zones.

Mode 4 - DHW Preheating: This mode is accomplished independently of the other three solar modes. Incoming city (makeup) water and recirculation return water are passed through a U-tube heat exchanger in the solar storage tank when the temperature of the water in storage exceeds the DHW heat exchanger inlet water temperature. From the heat exchanger the water returns to the 120-gallon DHW tank which contains an electric auxiliary heating element to supplement the solar preheat. Water from the DHW tank is continuously recirculated through the building's hot water lines and returned to the DHW tank via the heat exchanger or directly.

### II. PERFORMANCE EVALUATION

The system performance evaluations discussed in this section are based primarily on the analysis of the data presented in the attached computer-generated monthly report. This attached report consists of daily site thermal and energy values for each subsystem, plus environmental data.

The performance factors discussed in this report are based upon the definitions contained in NBSIR 76-1137, Thermal Data Requirements and Performance Evaluation Procedures for the National Solar Heating and Cooling Demonstration Program.

### A. Introduction

The Alabama Power Company solar energy site was in operation during the entire month of May. The solar energy system supplied approximately three percent of the combined loads for DHW, space heating and space cooling. Space cooling was the primary load for the month but none of this load was supported by solar energy since the solar heated water was not hot enough to support absorption cooling.

### B. Weather

The average ambient temperature for May was  $69^{\circ}F$  with an average daytime ambient temperature of  $73^{\circ}F$ . The long-term average temperature for May is  $70^{\circ}F$  for the Birmingham, Alabama area. With these mild temperatures, the heating and cooling loads are expected to be small for May. The total incident insolation on the collector array was 110.09 million Btu for an average of 1,518 Btu/ft<sup>2</sup>-day. This was below the May average of 1,896 Btu/ft<sup>2</sup>-day derived from long-term data for the Birmingham area.

### C. System Thermal Performance

<u>Collector</u> - Of the 110.09 million Btu of solar energy incident upon the collector array during May, 71.45 million Btu were incident when the collector pump (CP1) was operating. The system produced a net collection of 13.04 million Btu, which was 12 percent of the total incident radiation. The net collection of 13.04 million Btu was the result of 18.49 million Btu measured gain through the collectors reduced by a measured rejection of 5.45 million Btu. The relatively high level of energy rejection through the collectors was the result of frequent operation of the collector pump at times when insolation was too low for collection. The operating energy (collector pump power) for the collector subsystem was 2.22 million Btu during May.

Energy Collection and Storage Subsystem - The energy collection and storage subsystem (ECSS) includes the collector array, the solar storage tank and the lines connecting these elements to each other. The ECSS is connected to the load subsystems by supply and return lines. Figure 2 illustrates the ECSS and its energy flow paths. The net input to the ECSS through the collectors was 13.04 million Btu (18.49 million Btu collected, less 5.45 million Btu rejected). The output from the ECSS to the load subsystem connecting lines was 4.63 million Btu and the stored energy level experienced a drop of 0.61 million Btu. Therefore, the total loss of energy from the connecting lines and solar storage tank was 9.02 million Btu.

Storage - The measured input to the solar storage tank was 17.79 million Btu while solar energy was being collected. The total measured output from the solar storage tank was 8.61 million Btu. The measured temperature in the solar storage tank indicated a decrease of 0.61 million Btu in stored energy for the month. Therefore, the calculated loss through the walls of the storage tank was 9.79. The discrepancy between the loss in the storage tank walls and the total ECSS system losses will be discussed in the observations.

Domestic Hot Water Load - The DHW load calculation is based on the flow through the DHW heat exchanger and the temperature difference between the outlet and inlet of the DHW heat exchanger plus the auxiliary electrical energy input to the DHW heater tank. The average temperature maintained at the DHW tank outlet was 123°F during May. The total DHW load for the month was 1.72 million Btu, 90 percent of which was supplied by solar energy. Due to the nature of the DHW subsystem and the lack of measurement of the incoming cold water supply volume, this load includes both consumption and sustaining (loss) loads within the recirculating DHW subsystem. Since the operating energy in the DHW subsystem is due solely to the recirculating pump, no operating energy is charged directly to the solar energy system for DHW support.

Space Heating Load - The total measured space heating load for May was 1.21 million Btu, of which 1.16 million Btu, or 96 percent, were supplied by solar energy. The remaining 0.05 million Btu were supplied by the

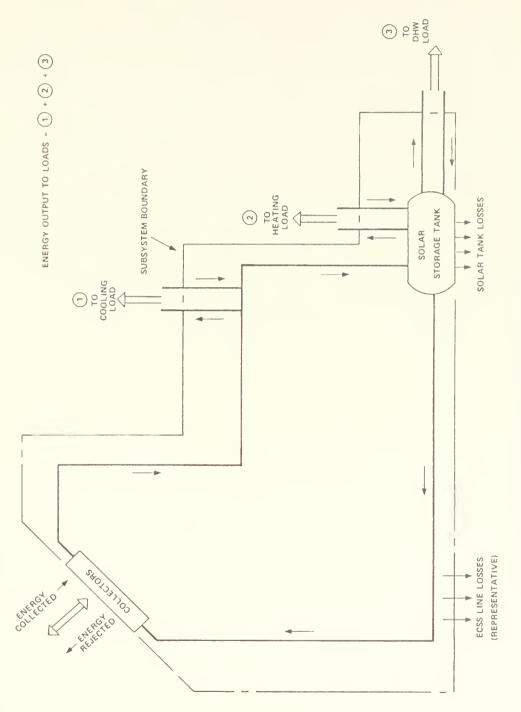


Figure 2. ALABAMA POWER COMPANY ECSS ENERGY FLOW SCHEMATIC

electric boiler. The total operating energy for the space heating subsystem was 0.17 million Btu of which 0.10 million Btu were charged directly to the solar energy system. The operating energy charged directly to the solar energy system was the pro-rata share of the circulation pump (HWP1, HWP2) power required to circulate the heated water through the space heating subsystem. Power to operate the air-handler fans was not charged against solar energy since that power would have been required regardless of whether a conventional or solar energy system was used.

Space Cooling Load - The total space cooling load for May was 85.04 million Btu. A negligible amount of this load was supported by solar energy due to the low temperature of the solar heated water available at the absorption chiller generator inlet. The absorption chiller was active on four days for a short period of time and the operating energy for space cooling charged to the solar energy system was 0.25 million Btu. The operation of the auxiliary electric chiller is summarized in the table entitled "Auxiliary Thermodynamic Conversion Equipment."

### D. Observations

A significant penalty was imposed on the solar energy system by the high percentage of energy rejected through the collectors. The space cooling mode of solar energy system suffered considerably, since the water temperature in the storage tank was not raised sufficiently to activate the absorption chiller. Control system improvements and basic repairs are needed to optimize solar energy collection and minimize rejection of energy through the collectors.

The seemingly high energy losses in the hot water storage tank are due to two factors. The first is the expected losses from the tank with two inches of polyurethane insulation. This calculates to be approximately 3.3 million Btu. Secondly, due to the placement of the collector control

sensor, collector pumps were activated every half-hour in the morning to determine an accurate collector outlet temperature. During the course of the month, this resulted in a rejection of approximately 6.5 million Btu of energy from the storage tank. Since this amount can only be determined indirectly, it does not enter into calculations for losses in the storage tank walls, giving an appearance of a greater loss from the storage tank walls than from the entire ECSS. This also explains why the storage tank temperature dropped 11°F when it appears that is should have gained energy. This difficulty is only temporary, since the collector control sensor should be relocated before August 1979.

### E. Energy Savings

A total electrical savings of 0.30 million Btu was calculated for the Alabama Power Company solar energy system. The savings calculations for DHW and space heating are based on the assumption that all load support provided by solar energy would have been provided by an equal amount of electrical energy. This load support is reduced by the amount of operating energy charged to solar hot water heating and solar space heating. The space cooling savings are calculated by obtaining the quotient of the load supplied by the absorption chiller divided by the coefficient of performance of a typical electric chiller (2.8) and subtracting the operating energy charged to solar (absorption) cooling. The total system savings is then calculated by summing the subsystem savings and reducing that sum by the amount of operating energy required by the ECSS.

### III. ACTION STATUS

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SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

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